

**Seminar for the California Geoprosessionals Association**

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*Soil Liquefaction During Earthquakes –  
The Cliffs Notes Version*

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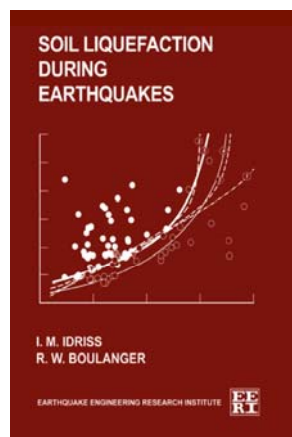
**Irvine, California  
June 11, 2009**

**Ross W. Boulanger**

*This seminar is based on:*

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- **Materials from the Monograph (MNO-12) published by EERI in 2008, and**
- **Materials presented at the EERI Seminars by I. M. Idriss & R. W. Boulanger in Pasadena, St. Louis, San Francisco & Seattle, on March 9, 11, 16 & 18, 2009, respectively.**



**SOIL LIQUEFACTION  
DURING EARTHQUAKES**

by  
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This monograph was sponsored by the  
Earthquake Engineering Research Institute  
with support from the Federal Emergency Management Agency

  
**EARTHQUAKE ENGINEERING RESEARCH INSTITUTE**  
MNO-12

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## *Plot summary*

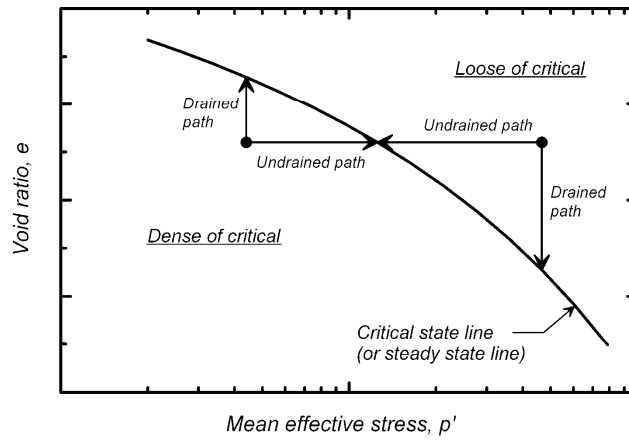
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- **Fundamentals of liquefaction behavior**
  - *Avoid confusion by being explicit with definitions.*
  - *The role of excess pore pressure diffusion.*
- **Triggering of liquefaction**
  - *New SPT and CPT curves: How they compare to others and when the differences can be important for you.*
- **Residual shear strength**
  - *New recommendations that include consideration of void redistribution effects.*
- **Lateral spreading and post-liquefaction settlements**
  - *Making decisions from incomplete information.*
- **Cyclic softening of clays and plastic silts**
  - *Choosing appropriate engineering procedures.*

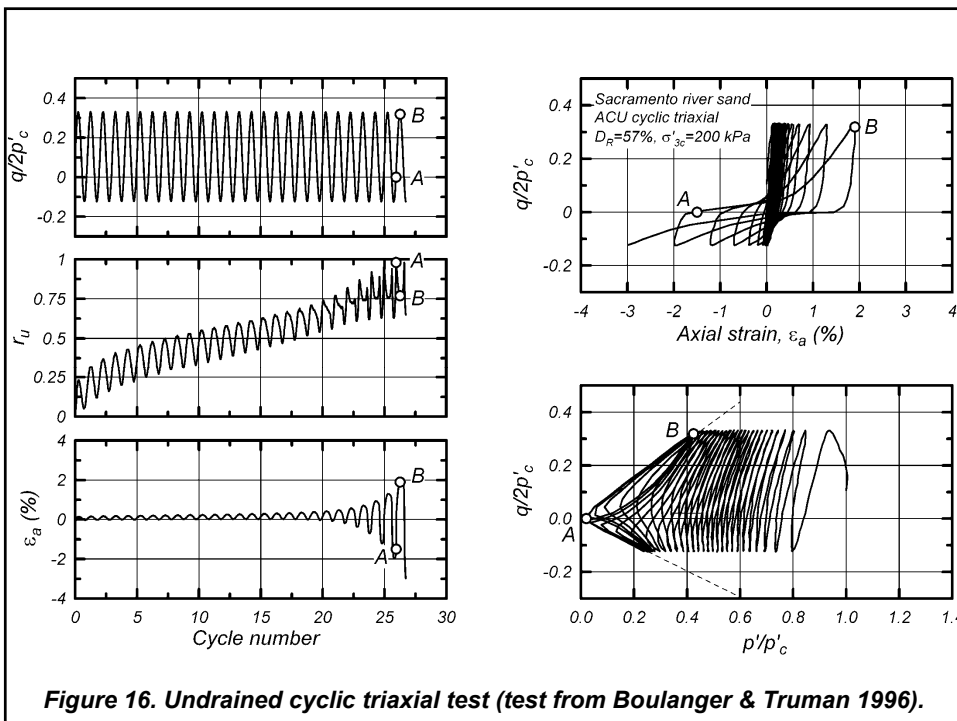
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## *Fundamentals of liquefaction behavior*

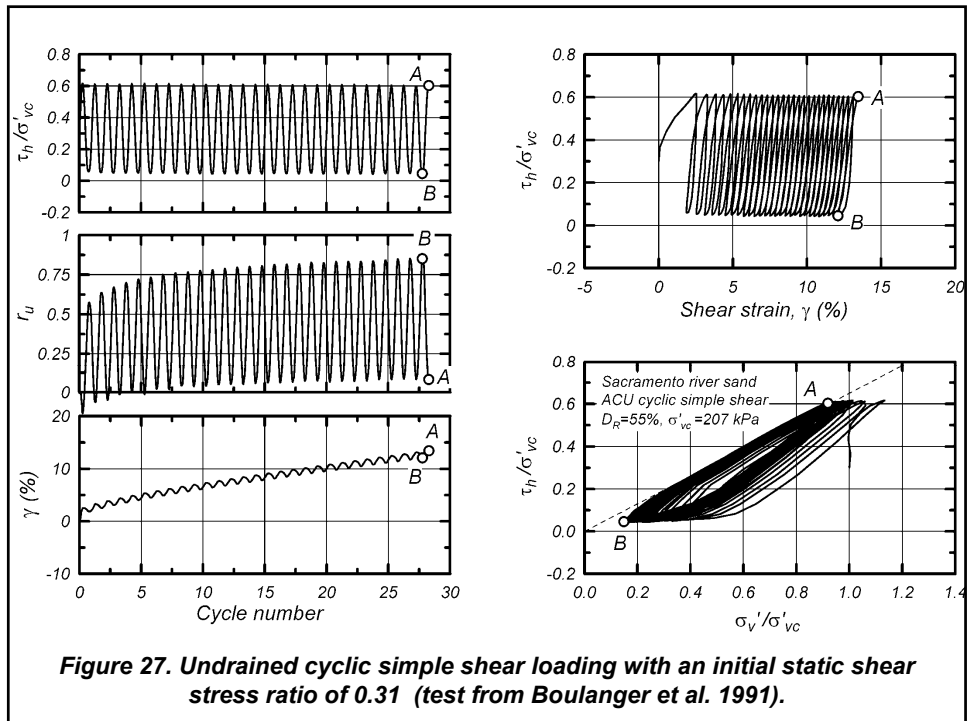
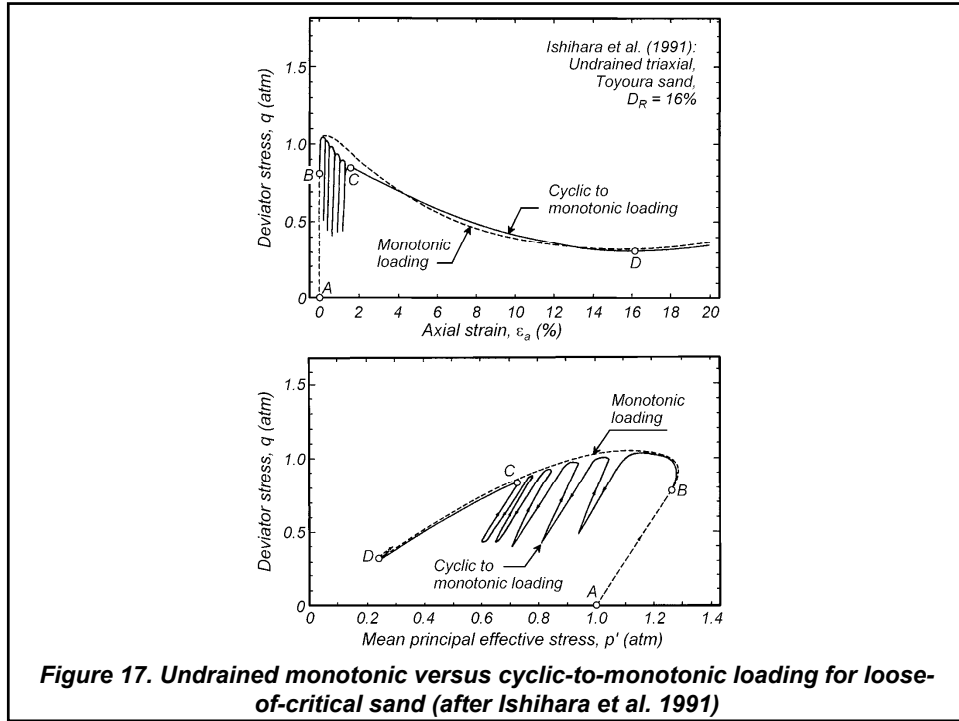
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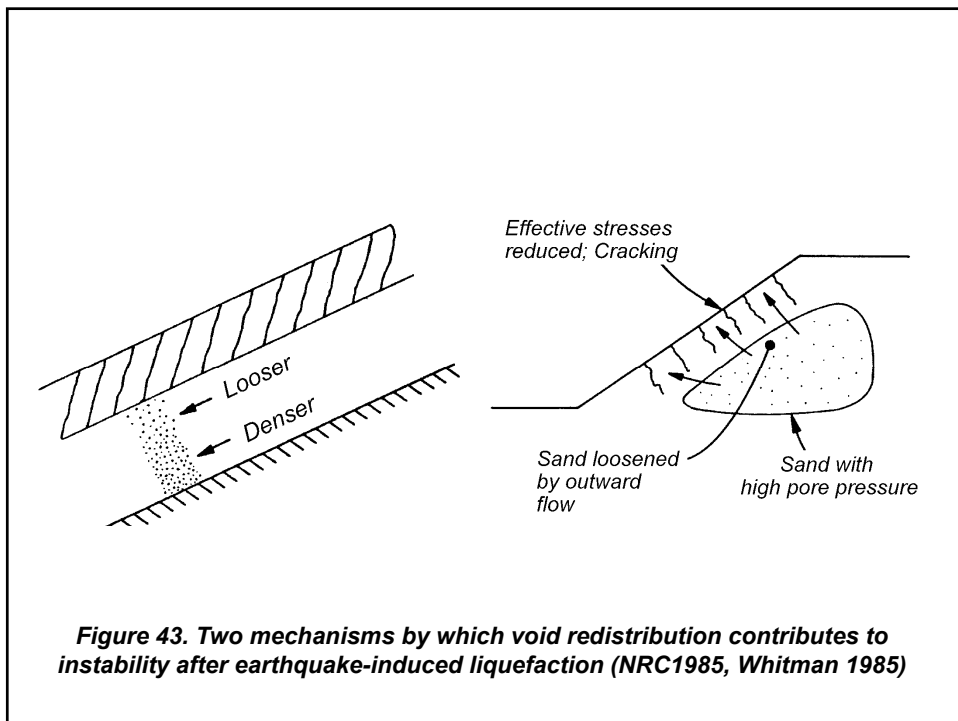
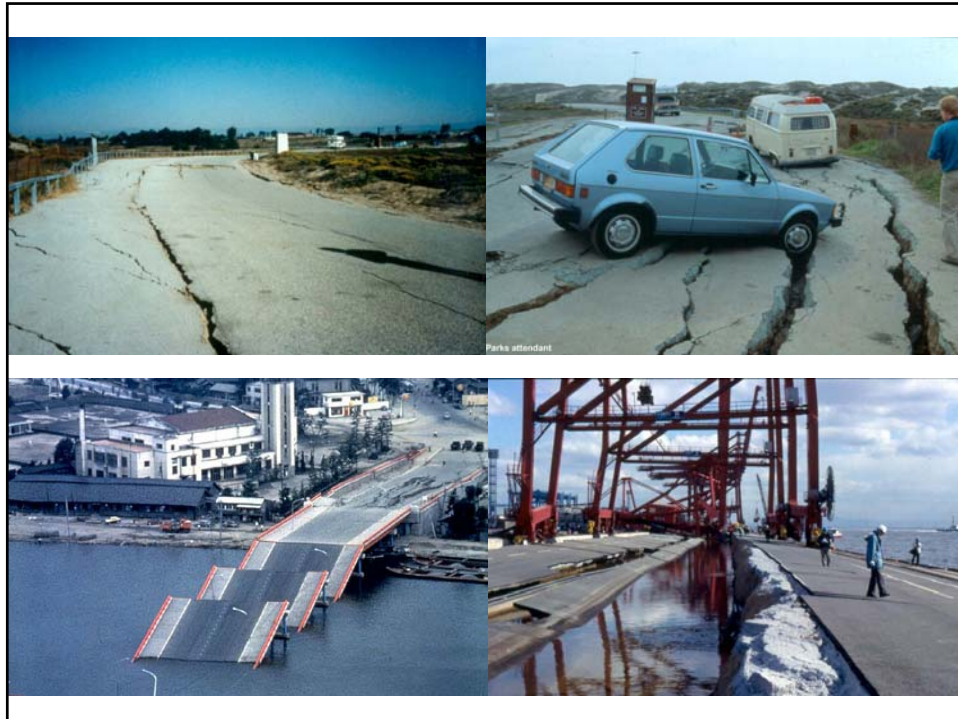


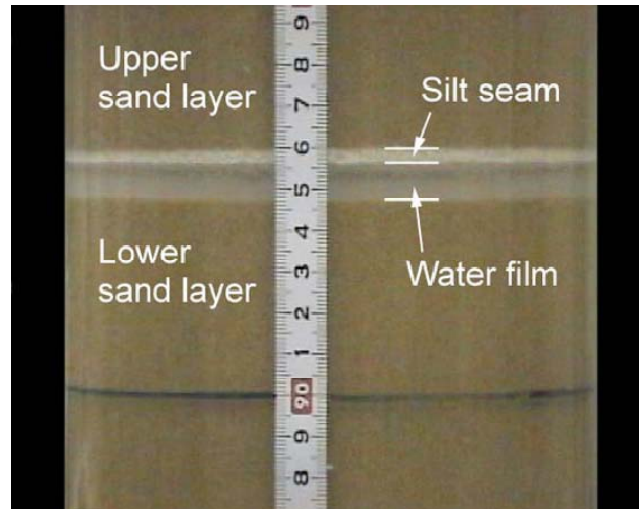
**Figure 8. Stress paths for monotonic drained loading with constant  $p'$  and undrained loading (constant volume shearing) of saturated loose-of-critical and dense-of-critical sands**



**Figure 16. Undrained cyclic triaxial test (test from Boulanger & Truman 1996).**

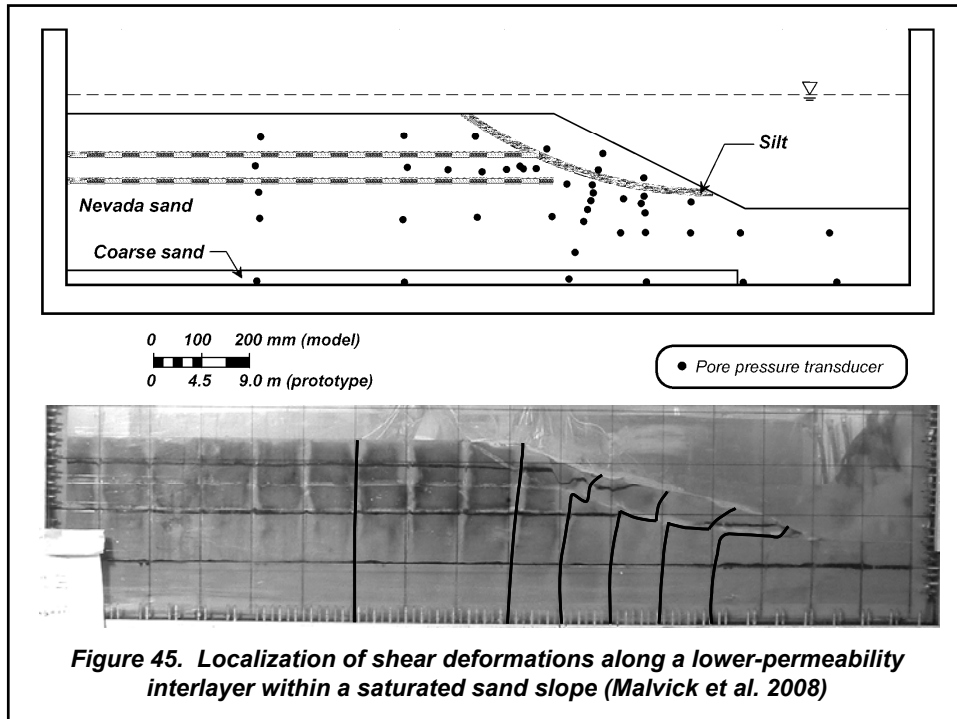






**Figure 44. A water film that formed beneath a silt seam in a cylindrical column of saturated sand after liquefaction (Kokusho 1999)**





### *Take home points*

- ***"Liquefaction" means different things to different people – use more specific technical terms to avoid confusion in technical discussions.***
- ***Critical state soil mechanics is a useful tool for appreciating the different behaviors of various soils over a range of densities and confining stresses.***
- ***In situ shear strengths can be affected by the diffusion of excess pore pressures during and after shaking.***

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## Triggering of liquefaction

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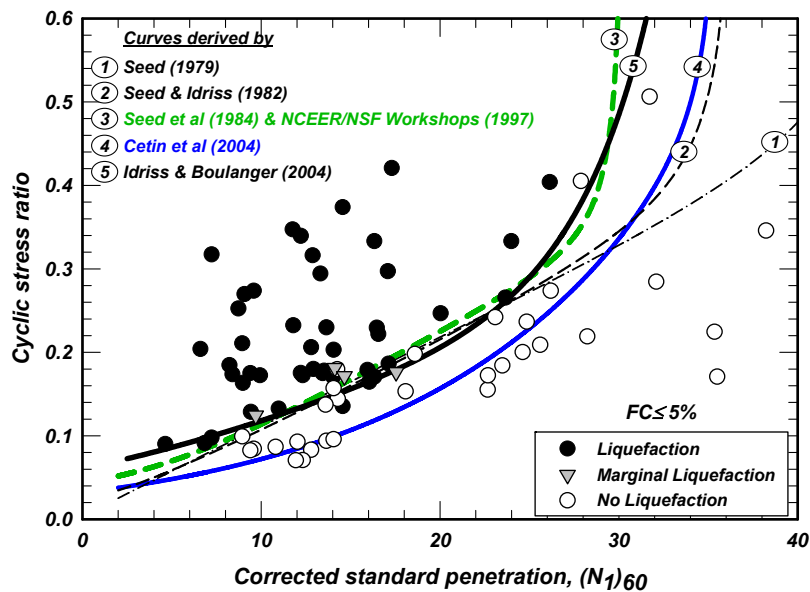
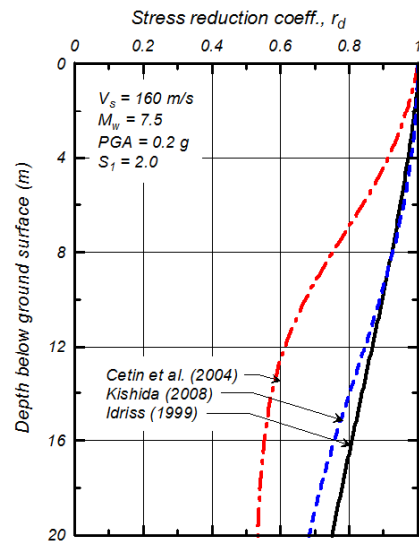
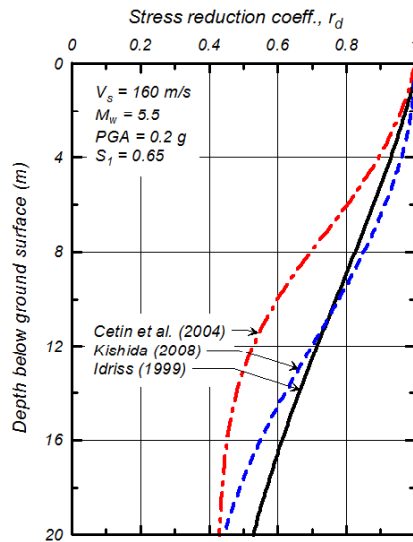
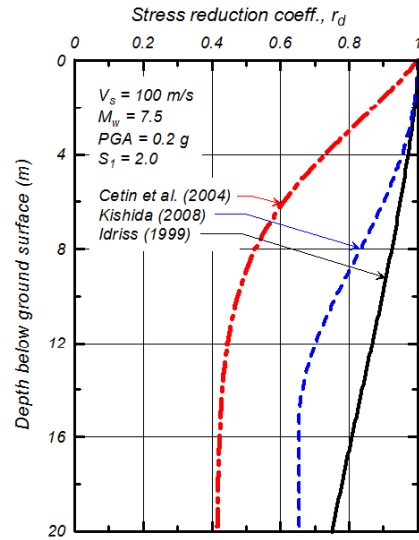
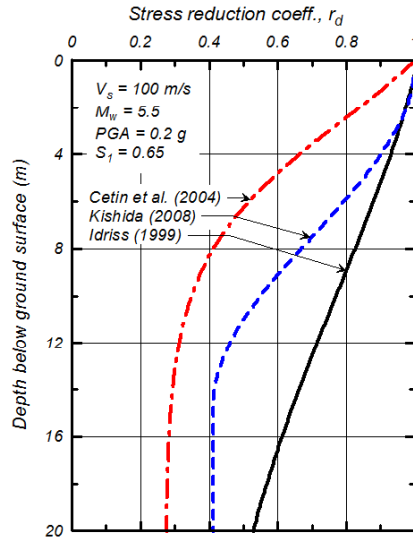


Figure 66 – Curves relating CRR to  $(N_1)_{60}$  for clean sands with  $M = 7\frac{1}{2}$  and  $\sigma'_{vc} = 1 \text{ atm}$ .



**A primary contributor to the differences between Cetin et al, NCEER and Idriss & Boulanger is the differences in  $r_d$ .**



Other notable sources of differences are:

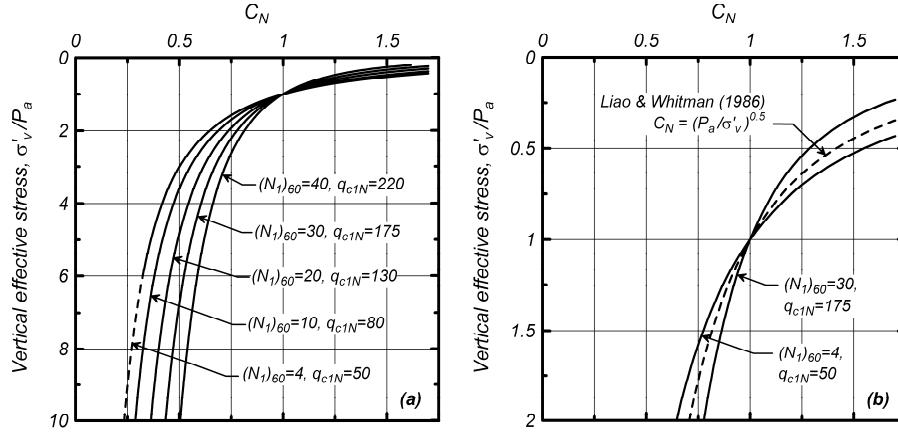


Figure 60 – Overburden normalization factor  $C_N$ : (a) dependence on denseness, and (b) simpler approximations often used at shallower depths.

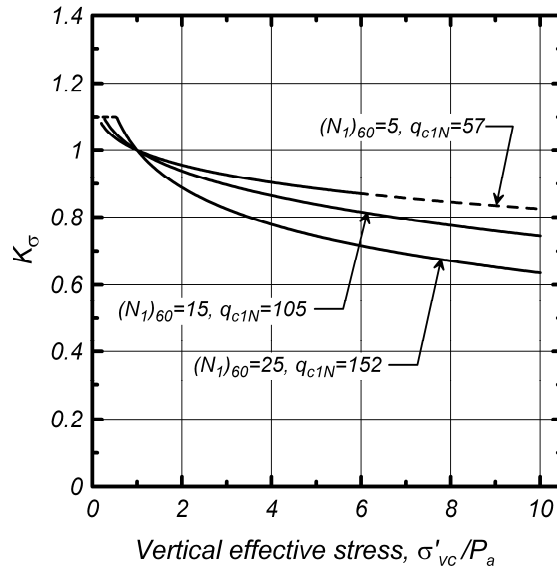
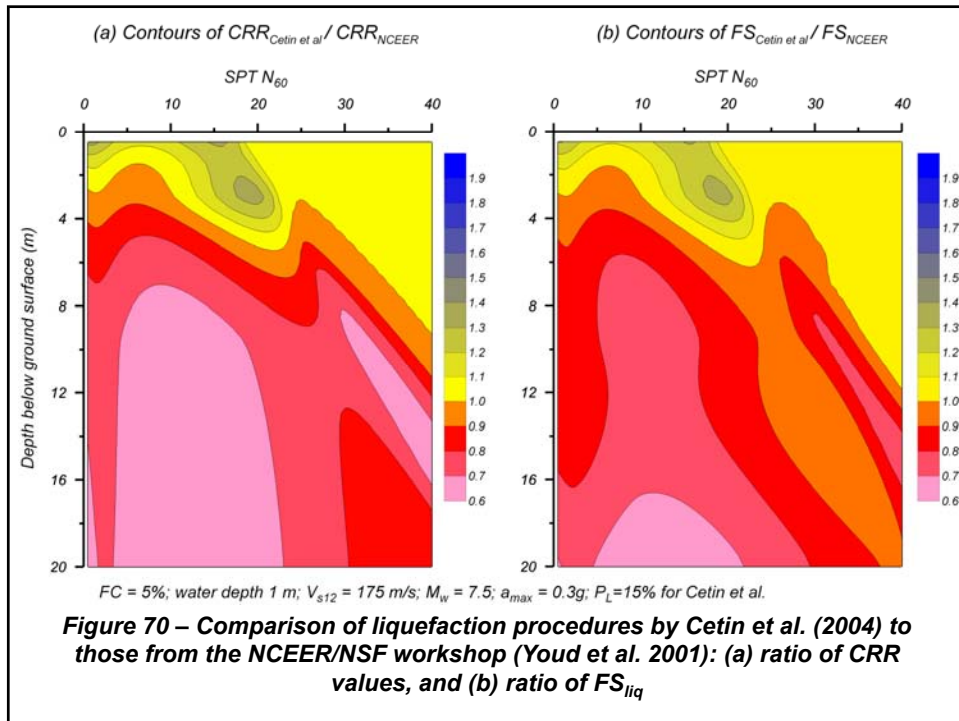
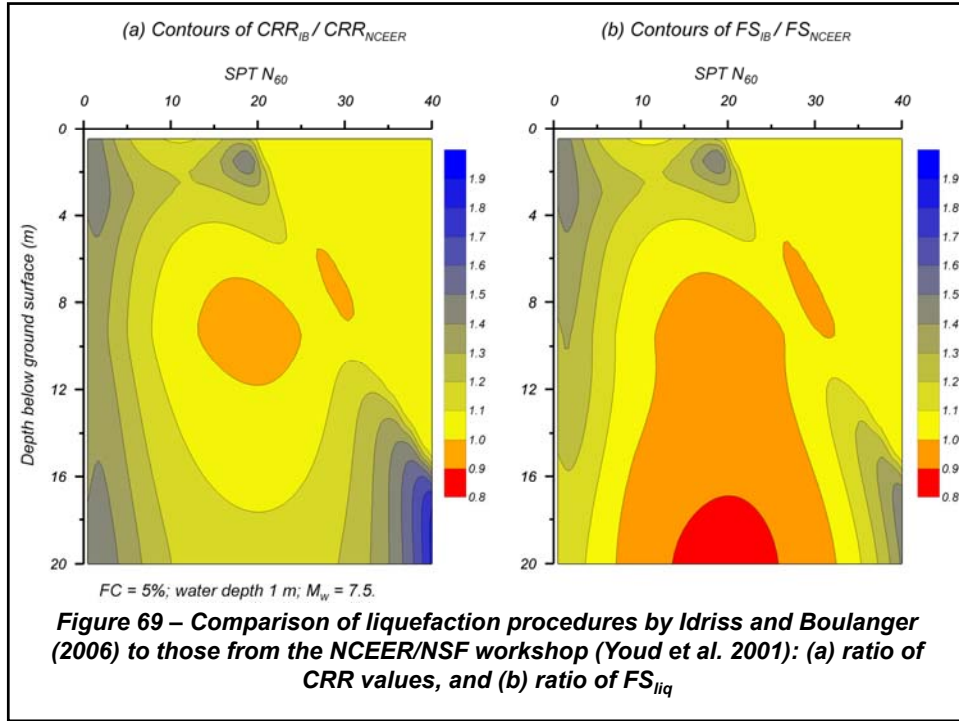
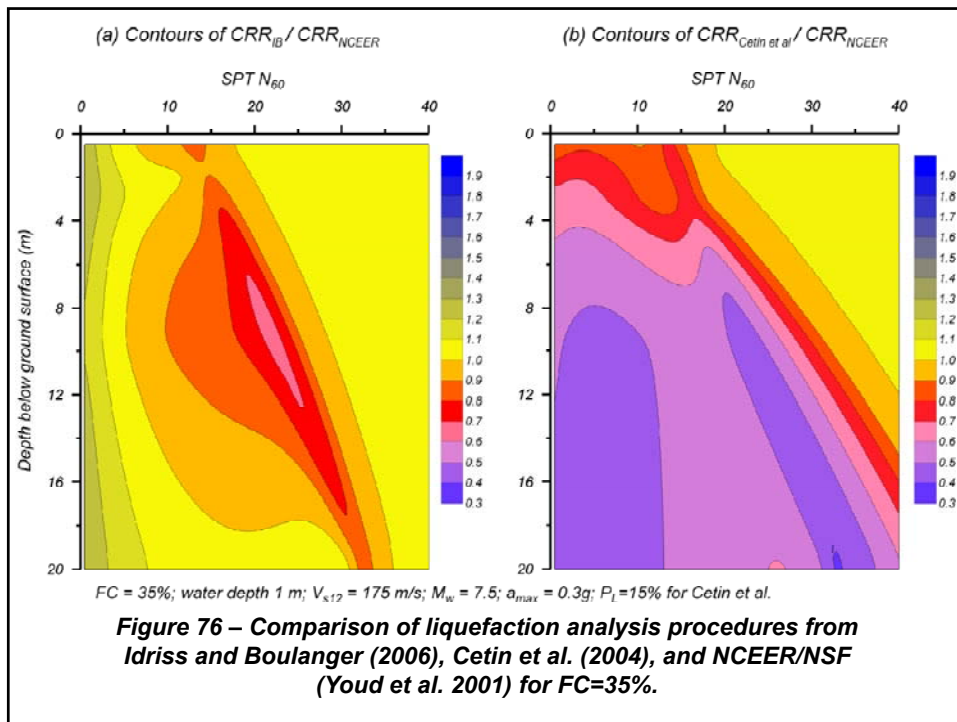


Figure 64 –  $K_\sigma$  relationships derived from  $\xi_R$  relationships (from Boulanger and Idriss 2004).





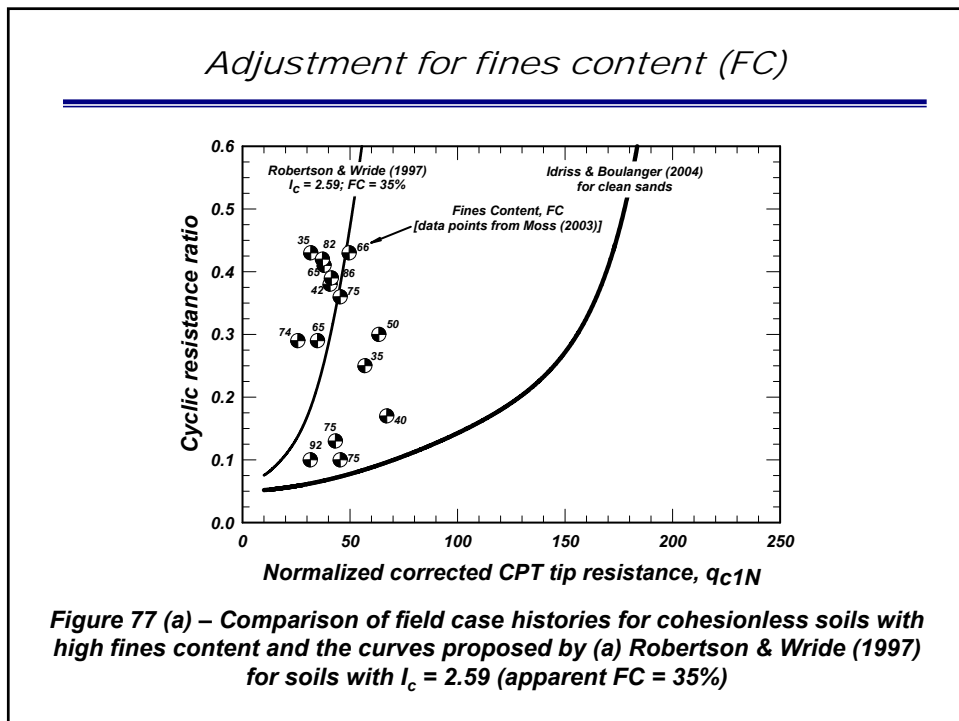
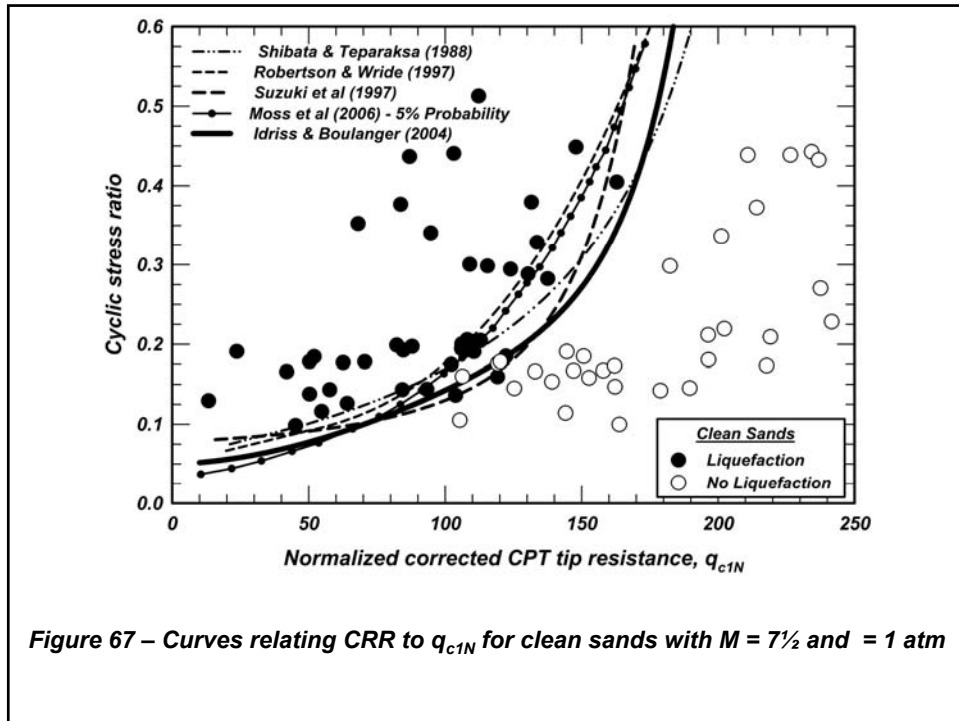
***Is there a depth, like 50 ft (or 15 m) below which we don't need to consider liquefaction as being possible?***

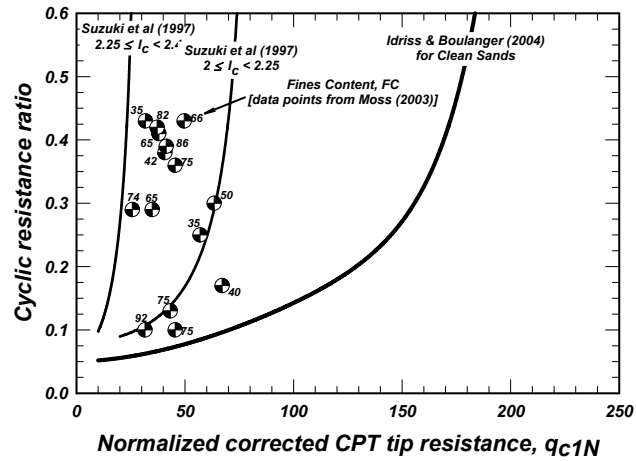
***EERI seminar participants***



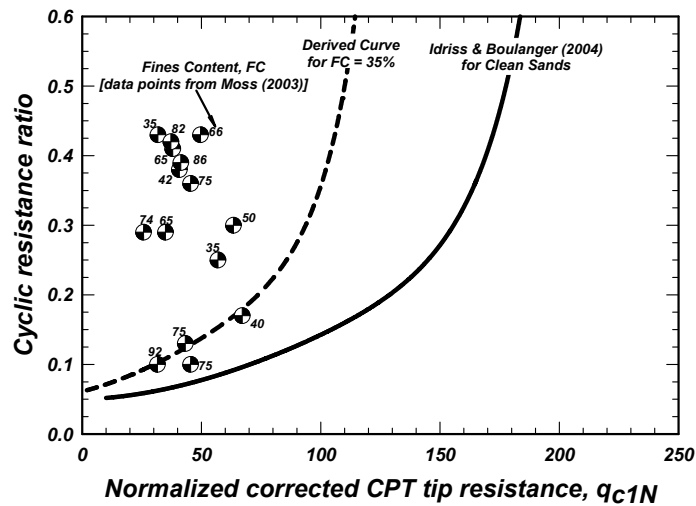
**Influence of depth on liquefaction:**

- **Mechanisms affecting:**
  - **Soil strengths**
  - **Seismic loads**
  - **Consequences**
- **Empirical observations – must have a theoretical basis for understanding how our experiences from one site may relate to another.**
- **Limitations in how analysis methods handle the role of depth.**





**Figure 77 (b) – Comparison of field case histories for cohesionless soils with high fines content and the curves proposed by (b) Suzuki et al (1997) for  $I_c$  values of 2.0 – 2.4**



**Figure 79 – Comparison of field case histories for cohesionless soils with high fines content and a curve recommended for cohesionless soils with FC = 35%**

### *Take home points*

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- **Curves relating CRR to  $(N_1)_{60}$  for clean sands and sands with non-plastic fines have largely stabilized.**
- **Curves relating CRR to  $q_{c1N}$  for clean sands are stabilizing, but the effects of fines content are subject to further refinements.**
- **Extrapolation of liquefaction correlations to depths larger than are covered empirically requires a sound theoretical basis.**

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### *Consequences of liquefaction:*

*Residual Shear Strength*

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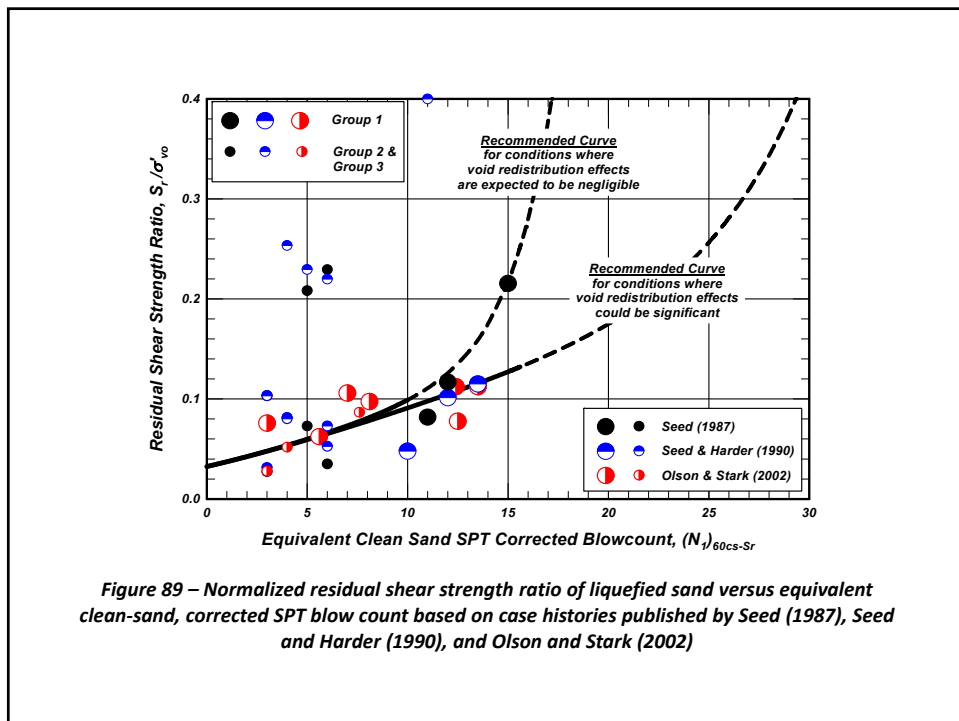
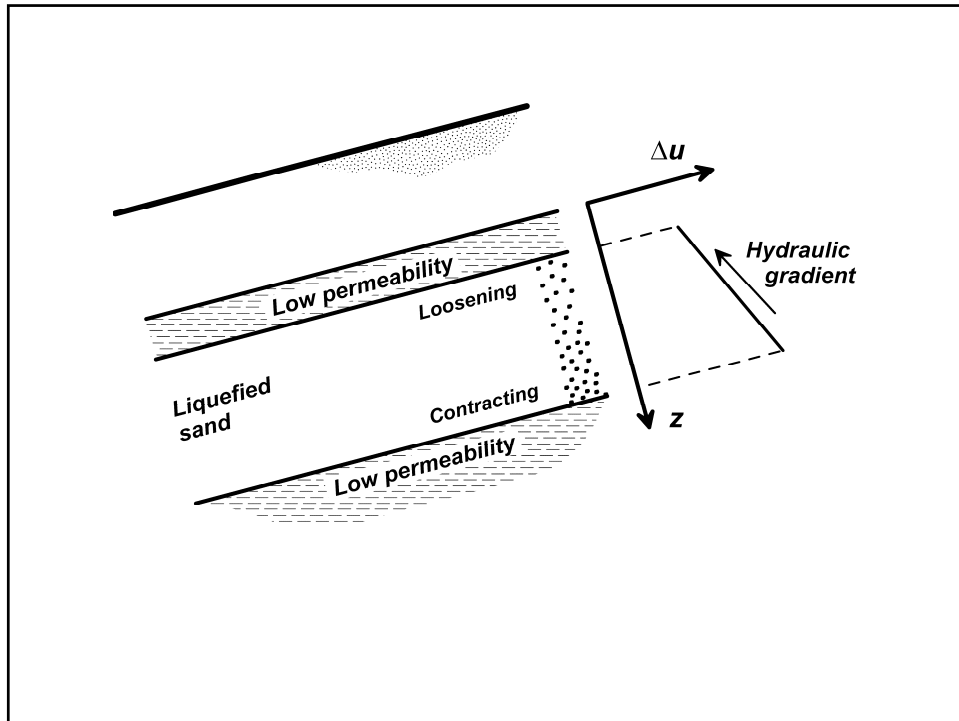


Figure 89 – Normalized residual shear strength ratio of liquefied sand versus equivalent clean-sand, corrected SPT blow count based on case histories published by Seed (1987), Seed and Harder (1990), and Olson and Stark (2002)

### *Take home points*

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- *An understanding of strength loss mechanisms is provided by laboratory testing and physical modeling studies.*
- *Case histories implicitly account for void redistribution.*
- *The relationships presented in the Monograph reflect the current understanding and capabilities for modeling this phenomenon.*
- *More work in this area is needed.*

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### *Consequences of liquefaction:*

*Lateral spreading and post-liquefaction  
reconsolidation settlements*

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## Lateral spreading analyses

- **Approaches**
  - **Empirical**
  - **Newmark sliding block analyses**
  - **Integrate potential strains versus depth**
  - **Nonlinear dynamic analyses**
- **None capture all the physical phenomena.**
- **Site characterization is a major source of uncertainty.**

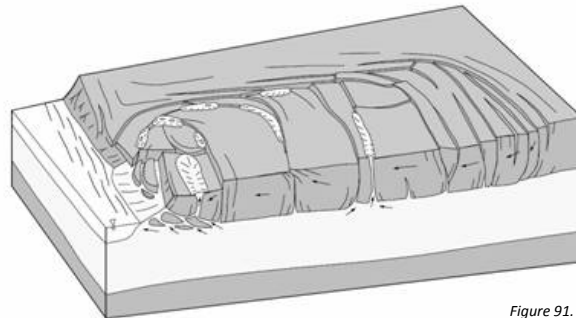
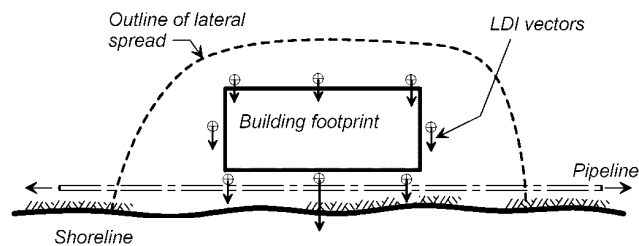
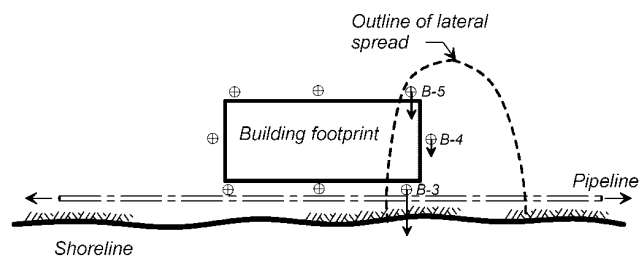


Figure 91.  
From Rausch 1997

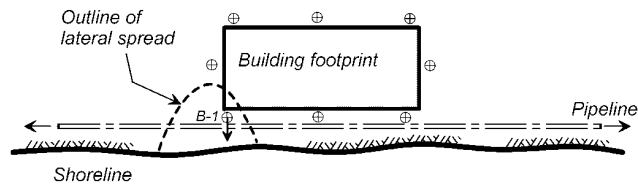


(b) Case I - liquefiable layer identified at all borings

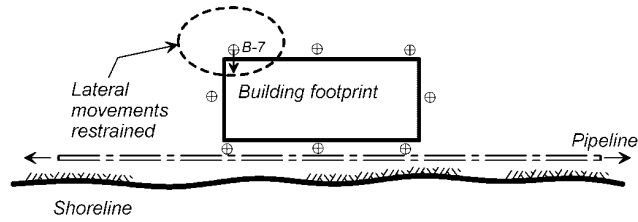


(c) Case II - liquefiable layer identified at borings 3, 4 and 5

**Figure 98. How LDI vectors may relate to the extent of lateral spreading**

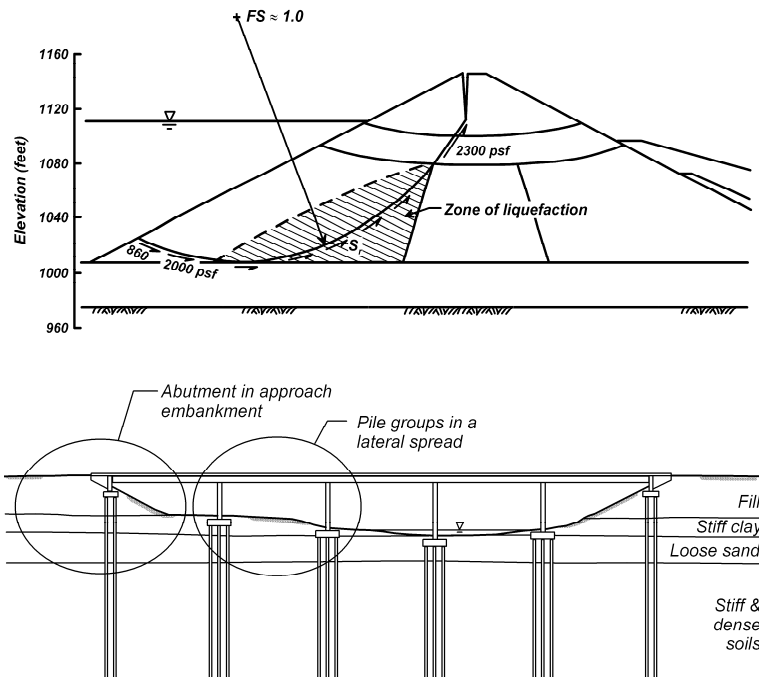


(d) Case III - liquefiable layer identified at boring 1 only



(e) Case IV - liquefiable layer identified at boring 7 only

**Figure 98. How LDI vectors may relate to the extent of lateral spreading**



### *Take home points*

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- ***Appropriate site characterization is essential for identifying and quantifying liquefaction hazards.***
- ***Simplified procedures for estimating liquefaction-induced ground deformations are inherently limited in their accuracy by the fact they cannot account for all the physical mechanisms or initial conditions.***
- ***The insights from various types of analyses, even if their accuracy is limited, can still guide effective decision making.***

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### *Cyclic softening in clays and plastic silts*

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## *What is liquefaction & what is cyclic softening?*



### *An interpretation problem*

- **Using "liquefaction" to describe ground failure in both sands and low-plasticity clays implies:**
  - a common behavior, and
  - a common set of engineering procedures.
- **If a silt/clay is deemed "liquefiable", it is common to use SPT- and CPT-based liquefaction correlations**
  - E.g., NCEER/NSF workshop (e.g., Youd et al. 2001)
  - Recommendations to sample and test "potentially liquefiable" silts/clays are often not heeded.

## *Reposing the question*

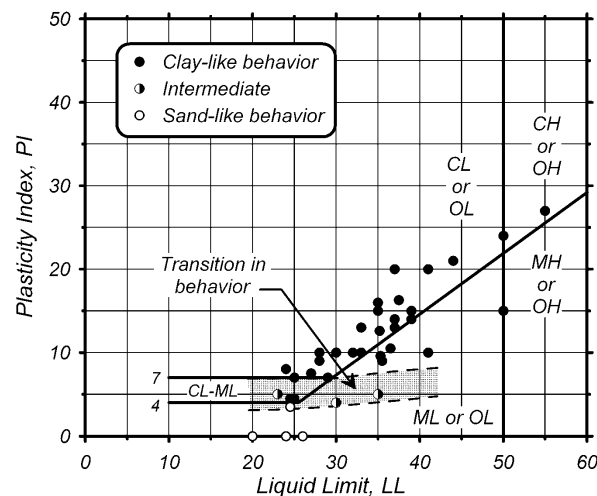
### ➤ Question:

- **What is the best way to estimate the potential for strength loss & large strains in different types of fine-grained soils?**
- **Or, what types of fine-grained soils are best evaluated using procedures modified from those for sands, versus procedures modified from those for clays?**

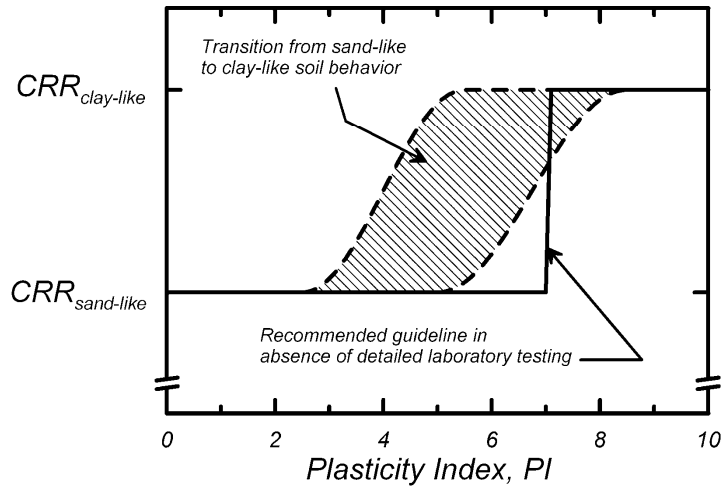
### ➤ Terminology:

- **"Sand-like" (or cohesionless) refers to soils that behave like sands in monotonic and cyclic undrained loading. Onset of strength loss and large strains is "liquefaction."**
- **"Clay-like" (or cohesive) refers to soils that behave like clays in monotonic and cyclic undrained loading. Onset of strength loss and large strains is "cyclic softening."**

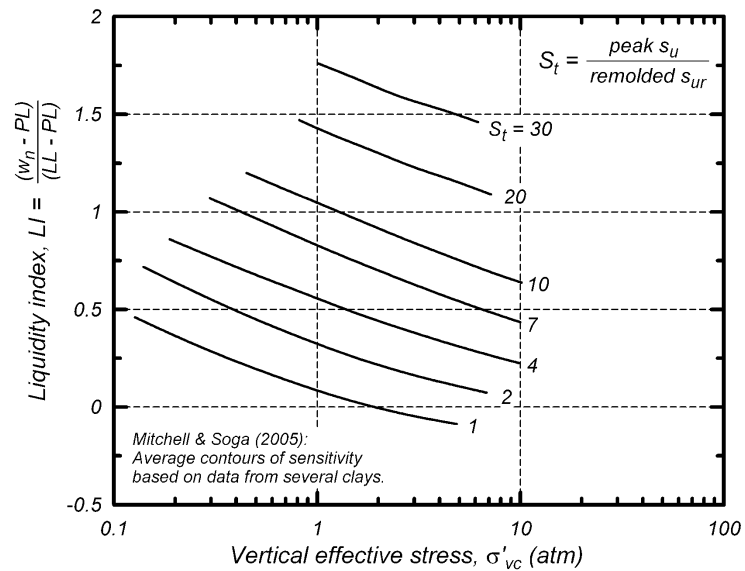
## *Atterberg limits of fine-grained soils exhibiting sand-like versus clay-like behavior*



- **Distinguishes between soils whose seismic behaviors are best evaluated using different engineering procedures.**



**Figure 135. Schematic of transition from sand-like to clay-like behavior for fine-grained soils**

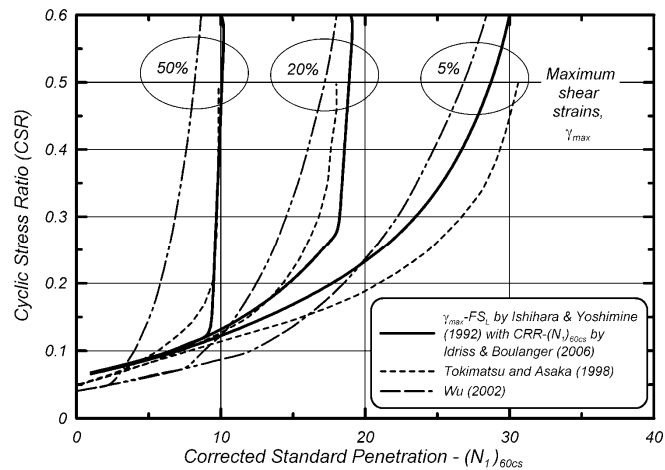


**Figure 136. Relationship among sensitivity, LI, and effective consolidation stress (after Mitchell and Soga 2005)**



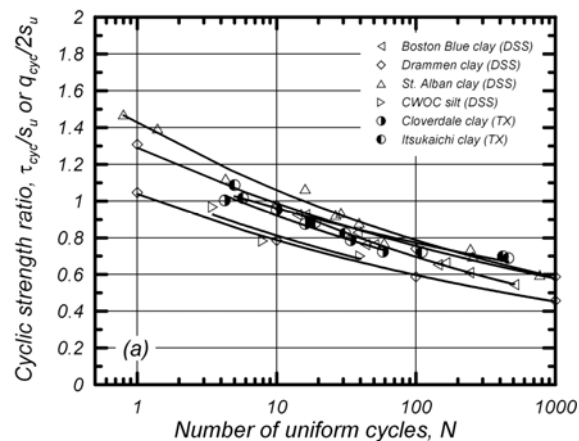
## "Liquefaction" procedures for cohesionless soils

- **Semi-empirical correlations based on in situ penetration tests.**
- **Consequences depend on relative density (e.g., bad if loose, not so bad if dense).**



## "Cyclic softening" procedures for cohesive soils

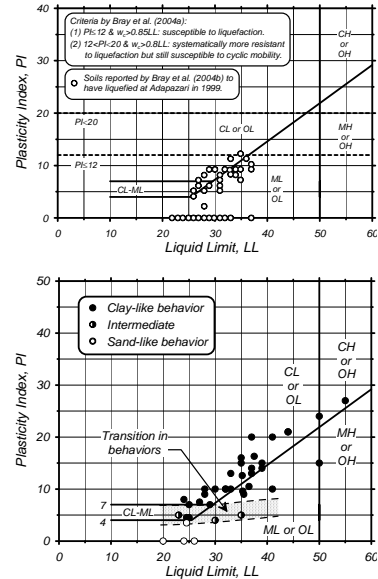
- **Procedures based on estimation of undrained shear strength (e.g., may include correlations, in situ tests, lab tests).**
- **Consequences depend on sensitivity (e.g., bad for quick clays, not so bad for insensitive clays; e.g., consider  $LI$  or  $w_p/LL$ ).**



## Comparing criteria – The common message

**Boulanger & Idriss (2004, 2006) and Bray et al. (2004, 2006).**

- **$PI < 4$ , no issue; Analyze using liquefaction correlations.**
- **$PI > 20$ , no issue; Analyze using procedures for clays.**
- **$4 \leq PI \leq 20$** 
  - **Agree soil may develop high  $r_u$ , lose strength, & deform.**
  - **Call it liquefaction, cyclic softening, or XYZ?**
  - **Issue: How best to evaluate XYZ behavior?**



## Take home points

- **Do not use the Chinese Criteria.**
- **Potential for cyclic softening of clay-like or cohesive fine-grained soils is best evaluated using procedures that are similar to, or build upon, established procedures for evaluating the monotonic undrained shear strength of such soils (e.g., Boulanger & Idriss 2004).**
- **Fine-grained soils transition from behavior that is best analyzed as "clay-like" versus "sand-like" over a narrow range of PI values.**
- **Fine-grained soils with  $PI \geq 7$  are best analyzed as clay-like. These criteria may be refined on the basis of site specific testing.**

